Abstract—Finite Set Model Predictive Control (FS-MPC) has many advantages, such as a fast dynamic response and an intuitive implementation. For these reasons, it has been thoroughly researched during the last decade. However, the wave form produced by FS-MPC has a switching component whose spread spectrum remains a major disadvantage of the strategy. This paper discusses a modulated model predictive control that guarantees a spectrum switching frequency in the linear modulation range and extends its optimized response to the overmodulation region. Due to the equivalent high gain of the predictive control, and to the limit on the voltage actuation of the power converter, it is expected that the actuation voltage will enter the overmodulation region during large reference changes or in response to load impacts. An optimized overmodulation strategy that converges towards FS-MPC’s response for large tracking errors is proposed for this situation. This technique seamlessly combines PWM’s good steady-state switching performance with FS-MPC’s high dynamic response during large transients. The constant switching frequency is achieved by incorporating modulation of the predicted current vectors in the model predictive control of the currents in a similar fashion as conventional Space-Vector Pulse Width Modulation (SV-PWM) is used to synthesize an arbitrary voltage reference. Experimental results showing the proposed strategy’s good steady-state switching performance, its FS-MPC-like transient response and the seamless transition between modes of operation are presented for a permanent magnet synchronous machine drive.

Index Terms—Predictive Current Control, Modulated Model Predictive Control.

I. INTRODUCTION

Finite Set Model Predictive Control (FS-MPC) has gained importance thanks to its conceptually simple implementation and very high transient performance. The basic principle of operation is the prediction of the future evolution of the system variables using a dynamic system model in order to select the actuation that optimizes this response. FS-MPC has been implemented successfully in multiple power converter topologies such as neutral point clamped converters (NPC) [1], [2], cascade H-bridge converters (CHB) [3], [4], flying capacitor converters [5], [6], three-phase two-level inverters [7], [8], multilevel converters [3], [9], and matrix converters [10], [11], among others.

However, FS-MPC has two important drawbacks. Firstly, the control strategy depends on the accuracy of the system model, which are not guaranteed due to parametric errors and the presence of unmeasured disturbances. Secondly, the discrete nature of the power converters imposes a very limited number of switching states for the FS-MPC strategy to apply, leading to steady-state error and a spread switching harmonic spectrum.

The switching harmonic spectrum depends on the compulsations of the converter’s power switches, which in FS-MPC is not guaranteed to occur at the fixed sampling frequency. This leads to a spread harmonic spectrum that, among other problems, makes filter and thermal design difficult [12]. In contrast to FS-MPC, current control techniques that use pulse width modulation (PWM) or space vector pulse width modulation (SV-PWM) have a fixed switching frequency and, therefore, their harmonic spectra are concentrated around the carrier frequency and its multiples. For this reason, several authors have proposed the use of continuous set MPC by including some type of modulation in the actuation of the predictive control [13]–[15]. In [13] the zero vector cost function value is used to determine the analogous actuation voltage required for current tracking. From that voltage reference, the duty cycles are calculated for each pair of adjacent active vectors. These times are then evaluated in a cost function to select the pair of active vectors to be applied. The proposed cost function does not consider the constraints on the duty cycles, which will lead to sub-optimal choices outside of the unconstrained linear modulation range. In [14], the control variable increments are considered constant during the time that a voltage vector is applied. Based on this assumption, the value of the voltage actuation required for zero current error is calculated considering the measured initial condition and the dynamic model of the system. In the overmodulation region, the constraints in the times are imposed after calculation of the unconstrained optimum times, leading to sub-optimal selections when the ac-
tuation is saturated. A slightly different approach is presented in [15]. Here, the error between the measured currents and the current references is used to calculate the times of the three vectors, two active vectors and the zero vector, that will result in zero tracking error. The main difference with the previously mentioned methods lies in that, in this method, the tracking error between the reference and the predicted model response is interpreted as an affine transformation, i.e. the combination of a linear transformation and a translation. This leads to an irregular and shifted current response hexagon. The triangular sub-region within the current error hexagon where the origin is located, i.e. the zero error point, can be determined a priori using vector mathematical properties in the transformed space. This reduces the computational effort and, for linear models, leads to the optimal results without an explicit cost function optimization. Furthermore, the method will lead to good results even for nonlinear systems provided that the state space model is differentiable and that the sampling time is small enough. Again, in the method proposed in [15], no optimization is attempted in the saturation region. All these works have two factors in common: the modulation of the actuation voltage and a dynamic response that achieves deadbeat performance in the linear zone, i.e. within the linear voltage actuation capability of the converter. Nevertheless, none of them present an optimized solution when the reference actuation lies outside of the linear modulation region. Operation in the overmodulation region is relevant when a high dynamics response is necessary, for example in servo applications. In this context, there are other works that propose switching to a different control strategy for the overmodulation region [16]–[19], which adds complexity.

The present work proposes a modulated model predictive control technique with optimized response, including in the overmodulation region. The optimized response in the linear modulation region is solved based on the method presented in [15]. The optimized modulated actuation is found with a system of equations in which the error between the reference and model prediction is modulated to zero. In the overmodulation region, the modulated combination of the two active vectors that result in the fastest dynamic response is found. Furthermore, it will be proved that when the reference tracking error is too large, the optimized solution is achieved with a single voltage vector, smoothly converging to the FS-MPC solution, which is known to be optimal for large transient errors. A geometrical criterion that minimizes the current error between the reference and the achievable current vectors, located in the limit of the irregular predicted current error hexagon, is proposed. This criterion is similar to the one proposed in [20] but is applied to the current error, i.e. in the transformed space of the predicted current errors proposed in [15], optimizing the system response rather than the actuation voltage. The proposed technique is experimentally tested as the internal current loop of a permanent magnet synchronous machine drive, showing PWM-like switching performance in steady state, FS-MPC-like transient performance and a smooth transition between both operation conditions.

II. ELECTRICAL SYSTEM MODEL

The modulated MPC strategy with optimized overmodulation is validated in an experimental setup with two types of load: a passive RL load and a permanent magnetic synchronous machine (PMSM). These loads are fed by a two-level voltage source inverter (2L-VSI). In this section, the mathematical models of the inverter and the different loads are presented. Furthermore, these models are discretized in order to implement the strategy in a digital control platform.

A. The Two Level Voltage Source Inverter

Using the spatial vector definition [21], it can be simply shown that the 2L-VSI generates eight voltage vectors, six of which are active vectors while two are zero vectors. The voltage vectors of the power converter, in a stationary $\alpha\beta$-frame, can be expressed as,

$$ v_{s_{\alpha\beta}} = v_{dc} \cdot \left[ \frac{2}{3} \cos \frac{2\pi}{3} e^{j\frac{2\pi}{3}} \right] \cdot S, $$

where $v_{dc}$ is the dc-link voltage, $S = [S_a \ S_b \ S_c]^T$ is the switching state vector of the converter and $S_x \in \{0, 1\}$ is the switching state of phase $x = \{a, b, c\}$. This converter voltage can be expressed in a synchronous $dq$-frame oriented with the angle $\theta$ by,

$$ v_s = v_{s_{\alpha\beta}} \cdot e^{-j\theta}. $$

B. Passive RL Load

The following is the model of the passive $RL$ load,

$$ L \frac{di_s}{dt} = v_s - R \cdot i_s, $$

where $i_s$ is the load current vector, $v_s$ is the output vector, $R$ is the resistance value of the load and $L$ is the inductance of the load.

A discrete model is necessary to model the continuous-time system in a digital device control platform. The RL load model is discretized with the forward-Euler approximation by,

$$ \frac{di_s}{dt} \approx \frac{i_{s}^{k+1} - i_{s}^{k}}{T_s}, $$

where $T_s$ is the sampling period.

C. Permanent Magnet Synchronous Machine

The model of the PMSM in a synchronous $dq$-frame oriented with the rotor position angle $\theta_r$ is as follows,

$$ x = [i_{sd} \ i_{sq} \ \omega_r \ \theta_r]^T, $$

$$ u = [v_{sd} \ v_{sq}]^T. $$

$$ \dot{x} = f(x, u), $$

$$ y = C \cdot x, $$

where

$$ T \frac{dx}{dt} = f(x, u), $$

$$ y = C \cdot x, $$

and

$$ f(x, u) = \begin{bmatrix} \dot{i}_{sd} \\ \dot{i}_{sq} \\ \dot{\omega}_r \\ \dot{\theta}_r \end{bmatrix}, $$

$$ u = [v_{sd} \ v_{sq}]^T. $$

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The modulated MPC strategy with optimized overmodulation is validated in an experimental setup with two types of load: a passive RL load and a permanent magnetic synchronous machine (PMSM). These loads are fed by a two-level voltage source inverter (2L-VSI). In this section, the mathematical models of the inverter and the different loads are presented. Furthermore, these models are discretized in order to implement the strategy in a digital control platform.
Current control load 

\[ \omega_s, \ \psi_m, J_m, B_m, \ \text{and} \ \alpha \beta \] 

The current error produced in the stator reference frame. The active vector can lie within the predicted current hexagon, i.e., operating in the overmodulation zone, as shown in Fig. 2(d).

A. Linear Modulation Zone

If the current reference lies in the linear modulation zone, then it is inside the triangle defined by \( v_{\text{opt}}, v'_{\text{opt}} \) and \( v_0 \). In this case, by modulating between these three voltage vectors, the current error can be made to average zero in a single sampling period. The problem is then reduced to obtaining the three times \( T_s \) with \( j \in \{0, 1, 2\} \) that solve the following system of equations,

\[
\begin{align*}
\sum_{j=0}^{2} \tau_j \cdot E_{d,j} &= 0, \\
\sum_{j=0}^{2} \tau_j \cdot E_{q,j} &= 0, \\
\sum_{j=0}^{2} \tau_j &= T_s,
\end{align*}
\]

where \( E_{d,j} \) and \( E_{q,j} \) are the errors in the d and q axis, produced by the zero vector \( (v_0) \), the optimum vector \( (v_{\text{opt}}) \) and the second optimum vector \( (v'_{\text{opt}}) \), as obtained with the cost function (10).

If the above equation system does not have a valid solution, i.e., one or more duty times are smaller than zero or greater
than $T_s$, the current reference is out of the linear modulation zone. Then, the converter cannot reach the current reference in a single sampling period and must enter overmodulation.

### B. Overmodulation with Two Active Vectors

When the current reference is located outside the predicted current hexagon, as shown in Fig. 2(c), the converter must be overmodulated. In this condition, the system of equations (13) is no longer applicable. This means that the current cannot reach the current reference in one sampling period due to limitations in the actuation voltage. In this case, the proposed overmodulation optimization finds the converter voltage that minimizes the error between the converter current and its reference subject to the limitations on the voltage actuation.

Solving the modulation problem in the predicted current space, as opposed to in the voltage space, allows for a simple minimization of the current error using a geometrical criterion. In fact, the minimum current error magnitude is the radius of the circumference centered in the reference that just touches the predicted current hexagon, while the resulting optimal current is given by the touch point, as shown in Fig. 3. When this circumference touches one side of the current hexagon, it does so tangentially, and the point can be found by the orthogonal projection of the current reference on the straight line defined by the two optimal current vectors, associated to $v_{opt}$ and $v'_{opt}$.

To find the optimized current error, the triangle formed by the current predictions and the current reference, depicted in Fig. 3(a), is considered. The angles $\alpha$ and $\beta$ of this triangle can be obtained with the following relationships,

$$\alpha = \arccos \left( \frac{x_1 \cdot x_3}{||x_1|| ||x_3||} \right),$$  
(14)

$$\beta = \arccos \left( \frac{x_2 \cdot x_3}{||x_2|| ||x_3||} \right),$$  
(15)

where,

$$x_1 = i^* - i_{p1}^,$$

$$x_2 = i^* - i_{p2}^,$$

$$x_3 = i_{p1}^ - i_{p2}^,$$

(16)

(17)

(18)

which are calculated according to the sector where the current reference is located, as indicated in Fig. 3(a) and (b). If the current reference is located in zone (1), i.e. the angles $\alpha$ and $\beta$ take values between $[0, \pi/2]$, then,

$$\tau_1 = T_s \left( \frac{||x_2|| \cos(\beta)}{||x_3||} \right),$$  
(19)

$$\tau_2 = T_s \left( \frac{||x_1|| \cos(\alpha)}{||x_3||} \right),$$  
(20)

$$\tau_0 = 0.$$  
(21)

The most relevant case for overmodulation with two active vectors is when the modulator is not deeply saturated, i.e. atleast one of the angles $\alpha$ or $\beta$ is small. In this condition, the equations (19) and (20) can be approximated by (22) and (23), reducing the computational load of the calculation of $\tau_1$ and $\tau_2$, respectively.

$$\tau_1 \approx T_s \left( \frac{\alpha}{\alpha + \beta} \right),$$  
(22)

$$\tau_2 \approx T_s \left( \frac{\beta}{\alpha + \beta} \right).$$  
(23)
C. Overmodulation by Only One Active Vector

If either $\alpha$ or $\beta$, calculated with the equations (14)-(15), respectively, is more than $\pi/2$, then the current reference is located in zone (2) of Fig. 3(b). In this case, the overmodulation strategy uses only one active vector with the following condition,

$$
\begin{align*}
\tau_1 &= T_s, \tau_2 = \tau_0 = 0 \quad \text{if} \quad \alpha > \pi/2 \\
\tau_2 &= T_s, \tau_1 = \tau_0 = 0 \quad \text{if} \quad \beta > \pi/2
\end{align*}
$$

(24)

It must be noted that the larger the current error, the higher the probability of the reference falling in zone (2), where only one voltage vector is applied for the complete sampling period. In this way, the operation smoothly transitions from PWM modulation at small current errors, to two-vector overmodulation in zone (1) and then to FS-MPC performance in zone (2). This ensures optimum performance in every mode of operation.

D. Flow Diagram

The proposed control strategy can be described by the flow diagram presented in Fig. 4. The steps are described below:

- Step 1, measurement of the load current $i_k^s$.
- Step 2, prediction of the current for $k + 1$.
- Step 3, prediction of the current for the instant $k + 2$ and evaluation of the cost function (10) for all possible vectors of the power converter.
- Step 4, identification of the two active voltage vectors that produces the lowest and second lowest values of the cost function evaluated in the previous step.
- Step 5, calculation of the duty times for the two active vectors found in the previous step and the zero vector, according to equation (13).
- Step 6, evaluation of the validity of the solution of equation (13), according to the subsection IV.A. If it is a valid solution, the flow diagram finishes, and the duty times that will be applied are those calculated in step 5. If the solution is invalid, the flow diagram continues to the following step.
- Step 7, calculation of the angles $\alpha$ and $\beta$ according to
V. VERIFICATION OF THE PROPOSED METHOD

A. Comparison With FS-MPC and PI-SVM

A verification of the proposed method is presented in this section by comparing it with the standard Finite-Set Model Predictive Control (FS-MPC) and a linear control, in this case proportional controller (PI) in synchronous dq-frame with space-vector modulation (PI-SVM). To make a fair comparison, the criteria presented in [22] were used. The proposed method used a PWM with an actualization of the duty cycles every 50 [$\mu$s]; this means that on average it applies 3 vectors per period. For this reason, the FS-MPC method has been implemented with a sample time of 17 [$\mu$s]. The PI-SVM scheme is the same as used in [22], and the linear controller is a classical PI controller tuned with the Magnitude Optimum (MO) criterion [23]. For the purpose of this comparison, a simple RL load has been chosen. The parameters of the load are presented in the Table I. Fig. 5 shows the dynamic behavior of the three methods when the quadrature current reference changes from 5 [A] to 10 [A]. The $dq$-current tracking reference is shown in Fig. 5(a); all the methods have a fast dynamics response. The times it took each method to reach 90 % of the reference were: 406 [$\mu$s] for the MMPC with optimized overmodulation, 374 [$\mu$s] for MS-MPC, and 500 [$\mu$s] for the PI-SVM. Both predictive methods are faster than the PI-SVM; meanwhile the FS-MPC is slightly faster than the proposed method. Initially, both predictive methods take a saturated actuation with only one active vector, which is the constant operational mode of FS-MPC. The small difference is in the overmodulation mode where the proposed method applies two active vectors to optimize the $dq$-current vector error. Under similar conditions FS-MPC results in a bigger vector error at the end of the sampling period, overshoot the reference. However, for the same reason, the current reaches the reference slightly earlier. The phase currents are presented in the Fig. 5(b), where all the methods have a good sinusoidal wave-form. Fig. 5(c) shows the duty cycles calculated for all the methods. FS-MPC applies one vector per period, so its duty cycles are 0 or 1. The proposed method and PI-SVM have a similar behavior in steady-state, which is regarded as a very good quality of the proposed method. In dynamic state, the MMPC with optimized overmodulation reaches a saturated actuation, similar to FS-MPC, that allows it to obtain a fast response; then it has a soft transition to SVM mode in steady-state.

Fig. 6 presents the output current spectrum for all the methods in steady-state when operating with a reference of 10 [A]. As expected in techniques that use PWM, the proposed method and PI-SVM have a spectrum concentrated around $f_{sw}$ and 2$f_{sw}$ and higher multiples of $f_{sw}$ (not shown), while the standard FS-MPC has a distributed spectrum, which is typical of this method. The total harmonic distortion values for the three methods are: 1.13 % for the MMPC with optimized Overmodulation, 1.85 % for FS-MPC and 1.22 % for PI-SVM.

B. Sensitivity Analysis

The proposed method is analyzed in the presence of parameter variations. The electric load parameters are varied within ±50% of their nominal values (Table I). The total harmonic distortion (THD) and the magnitude of the total steady-state vector error are considered as performance indexes. For simplicity, only one parameter is varied at a time. Fig. 7(a) shows the results of the resistance variation. The THD has an almost linear variation from 0.97 % to 1.33 %, while the total steady-state error grows quasi-symmetrically as the resistance deviation increases. Fig. 7(b) shows the effect of the inductance variation. The THD has relatively high values for under-estimated inductance values, with a THD of 15.15 % when the inductance is 50 % of the nominal value. For the over-estimation of inductance values, the performance indexes do not present significant increases. In general, the resistance variations have a larger effect in the error, while the inductance under-estimation increases the THD.

VI. EXPERIMENTAL RESULTS

The proposed modulated model predictive control with optimized overmodulation was tested experimentally with two different types of loads.

The experimental setup is shown in Fig. 8. The power converter is a laboratory prototype 2L-VSI, and the control platform used is a TMS320C6713 DSP. This processor takes the current phase measurements and performs the modulated model predictive control calculations, sending the gate switching control signals by optical fiber. The output power phases of the converter are connected to the loads. Initially, an RL load is used to illustrate the efficacy of the control principle. Then, a PMSM test bench is used as a realistic application environment. The machine test bench is composed of a PMSM and a DC loading machine. Both machines are mechanically coupled, and the armature of the DC machine is fed by a controlled DC power supply for speed regulation. A sampling
Fig. 5. Simulation performance comparison of Modulated Model Predictive Control (MMPC) with optimized overmodulation, standard Finite-Set Model Predictive Control (FS-MPC) and PI controller in $dq$–frame with Space Vector Modulation (PI-SVM). (a) $dq$-current control; (b) Phase currents; (c) Duty cycles.

Fig. 6. Phase output current spectrum of (a) Modulated Model Predictive Control (MMPC) with overmodulation optimization, (b) Standard FS-MPC, and (c) PI-SVM.

Fig. 7. Sensitivity analysis of the proposed method. (a) Resistance variation; (b) Inductance variation.

The time of $T_s = 50[\mu s]$ is used for the implementation of the control strategy. The PWM frequency of $f_{sw} = 10[kHz]$ is achieved by using symmetrical PWM pulses. The sampling frequency for the proposed method is the same as that used for the asymmetric PI-SVM modulation, i.e. double the carrier frequency of 10 kHz, resulting in a sampling frequency of 20 kHz. This is substantially lower than the sampling frequency required by FS-MPC, due to the higher volt-second resolution obtained with PWM respect to that obtained by applying a constant voltage during a whole sampling period. In this sense, the computation effort of the proposed method is significantly lower than that of FS-MPC and only slightly higher than that of the PI control with SV-PWM modulation. The parameters of the RL load and PMSM are presented in Table I.

A. RL Load

The results for current control on the RL load are shown in Fig. 9. A relatively high impedance RL load is used to illustrate the operation of the proposed method in saturation. The transition between the linear modulation and overmodulation zones, using one and two active vectors, is shown in Fig. 9. In Fig. 9(a), the current control in $dq$–frame has a
good steady-state performance and a fast dynamic response when the reference changes. In fact, section IV-B shows that the time taken to reach the new current reference is indeed minimal. The phase currents are shown in Fig. 9(b); these currents have a sinusoidal waveform without a perceptible harmonic distortion. The duty cycle of the three phases of the power converter is presented in Fig. 9(c). These waveforms include the typical common mode of space vector voltage modulation, indicating that the utilization of the DC-link is also maximized in the proposed strategy. Also, the duty cycle’s waveforms show some distortion in the zero crossing of the currents. This distortion compensates, via current feedback, for the volt-seconds lost due to dead-time and device voltage drop, effectively cancelling their effects in the currents, as can be appreciated in Fig. 9(b). A signal that represents the location of the current reference in terms of linear or saturated zone of operation is shown in Fig. 9(d). Observing Fig. 9(c), it is also possible to identify when the modulation strategy is operating in the linear modulation zone or in either of the two overmodulation zones: when only one active vector is applied by saturation of the three duty cycles (or overmodulation in zone 2) and when two active vectors are used by saturation of two duty cycles (overmodulation in zone 1). When overmodulation starts, all the duty cycles of all three phases have a binary value (\(d_a=0\), \(d_b=1\), \(d_c=1\)), and then, phase \(b\) takes a variable duty cycle, producing a modulation between the switching state \([0\ 1\ 1]^T\) and the state \([0\ 0\ 1]^T\). This result clearly demonstrates the FS-MPC-like performance in response to large errors, the PWM operation in steady state and the smooth transition between modes.

### B. PMSM Load

The steady-state behavior of the modulated model predictive control applied to a PMSM is presented in Fig. 10. In this set-up, the shaft of this machine is directly attached to the shaft of a loading DC machine whose speed is kept relatively constant by means of a constant armature voltage. The \(d_q\) currents and their references are shown in Fig. 10(a); the quadrature current has good control with neither an observable steady-state error nor significant ripple. On the other hand, an observable steady-state error is present in the direct current control. This steady-state error may be due to modeling errors in the predictive model which may be parametrical errors in the machine model such as in the magnitude of the back-EMF or un-modeled effects such as nonlinearities of the converter produced by a device voltage drop or dead-time. Model predictive control is always sensitive to model inaccuracies, but this problem is more evident in the modulated model predictive strategy than in FS-MPC due to the lower switching noise. Fig. 10(b) shows the oscilloscope capture of the phase currents, which have a sinusoidal wave-form with the characteristic switching ripple of PWM. The total harmonic distortion (THD) is 3.34 %. The THD for different \(i_q^*\) current reference levels are presented in Table II; the THD’s are lower than 4.5 % in all cases. The current spectrum of the phase current of Fig. 10(b) is presented in Fig. 11. The spectrum has switching harmonics that are concentrated around the fixed carrier frequency and its multiples, as is characteristic of currents produced by PWM modulation.

<table>
<thead>
<tr>
<th>Current reference [A]</th>
<th>THD [%]</th>
</tr>
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<tbody>
<tr>
<td>6</td>
<td>2.87</td>
</tr>
<tr>
<td>8</td>
<td>3.3</td>
</tr>
<tr>
<td>10</td>
<td>3.34</td>
</tr>
<tr>
<td>12</td>
<td>4.12</td>
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Finally, a dynamic response of the modulated model predictive control method is shown in Fig. 12. The quadrature current reference changes from \(-5\) [A] to 10 [A]. A very fast dynamic response is observable. However, the setting of the current at the reference does show a low amplitude, low frequency oscillation which may be due to transient variations of the system speed caused by poor speed regulation in
the loading machine. The phase currents in Fig. 12(b) are sinusoidal without any significant harmonic distortion and show an extremely fast dynamic response.

VII. CONCLUSIONS

A modulated model predictive control with optimized overmodulation has been proposed in this work. In steady state, the constant switching frequency achieved with this technique is an important advantage because it solves the problem of distributed harmonic content in FS-MPC. The modulated voltage actuation of the power converter improves the tracking of the current references and achieves the desired concentrated PWM switching harmonics. On the other hand, the overmodulation optimization introduced in this work improves the performance of the method during large demand changes, achieving minimum time transients. With this optimization, the inherent voltage error generated when the equivalent reference is located outside of the actuation capability of the inverter is such that the resulting current error is minimized using a simple geometrical consideration. This optimized overmodulation guarantees the fastest dynamic response possible, achieving the same transient performance as FS-MPC for large transients. Furthermore, the use of overmodulation with two active

REFERENCES

Fig. 12. PMSM’s current dynamic response to an inversion of $i_{dq}$ reference. (a) Current control in $dq$-frame; (b) Phase currents.
Jose R. Rodriguez (M’81-SM’94-F’10) received the engineer degree in electrical engineering from the Universidad Técnica Federico Santa María, in Valparaíso, Chile, in 1977, and the Dr.-Ing. degree in electrical engineering from the University of Erlangen, Erlangen, Germany, in 1985.

In 1977, he became a Full Professor in, and the President of the Department of Electronics Engineering, Universidad Técnica Federico Santa María. Since 2015, he has been the President of the Universidad Andrés Bello, Santiago, Chile. He has co-authored two books, several book chapters, and more than 400 journal and conference papers. His research interests include multilevel inverters, new converter topologies, control of power converters, and adjustable-speed drives.

Dr. Rodriguez is member of the Chilean Academy of Engineering. He is the recipient of a number of best paper awards from journals of the IEEE. He was the recipient of the National Award of Applied Sciences and Technology from the Government of Chile in 2014. He was also the recipient of the Eugene Mittelmann Award from the IEEE Industrial Electronics Society in 2015.

Pericle Zanchetta (M’00-SM’15) received his MEng degree in Electronic Engineering and his Ph.D. in Electrical Engineering from the Technical University of Bari (Italy) in 1993 and 1997 respectively. In 1998 he became Assistant Professor of Power Electronics at the same University. In 2001 he became lecturer in control of power electronics systems in the PEMC research group at the University of Nottingham - UK, where he is now Professor in Control of Power Electronics systems.

He has published over 300 peer reviewed papers, he has been Chair of the IEEE-IAS Industrial Power Converter Committee IPCC and he is now Vice-Chair of the IEEE-IAS Industrial Power Conversion Systems Department (IPCSD). His research interests include control of power converters and drives, Matrix and multilevel converters.

Shafiq A. Odhano (S’13-M’15) received MSc degree in Electrical Engineering from Politecnico di Torino (Italy) from where he obtained his PhD degree in Power Electronics, Machines and Drives in 2014.

He worked with the Politecnico di Torino as a postdoctoral research fellow and is currently with the University of Nottingham (UK) in the same role. Dr. Odhano’s research interests include high performance control of servodrives, model predictive control of power converters and self-commissioning of ac motor drives.

Dr. Odhano was the recipient of IEEE-IAS Prize Paper Award for the year 2015.